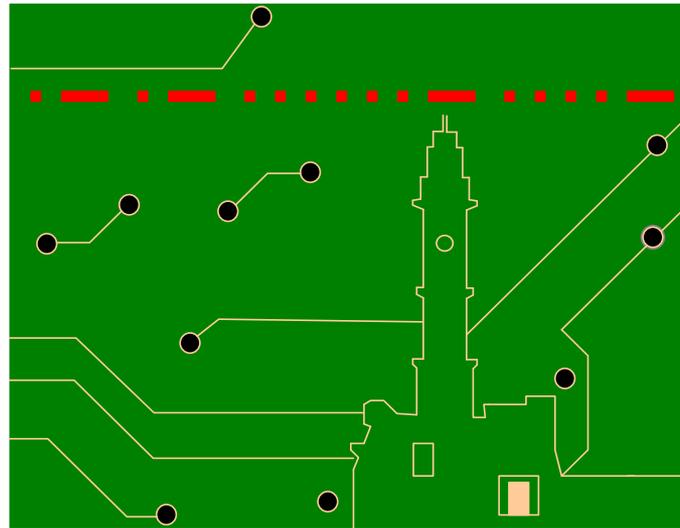


ΤΗΛ412 Ανάλυση & Σχεδίαση (Σύνθεση) Τηλεπικοινωνιακών Διατάξεων

Διάλεξη 4



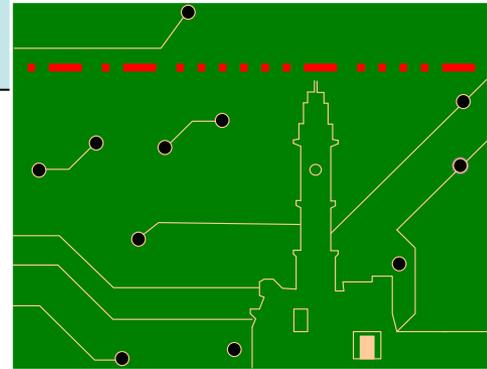
Άγγελος Μπλέτσας

Σχολή ΗΜΜΥ Πολυτεχνείου Κρήτης, Φθινόπωρο 2014

Lecture 4: Receiver Architectures (Part A)

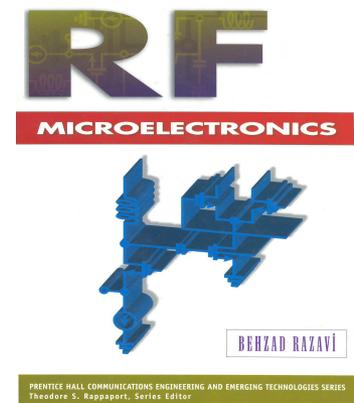
Today,

- Filter Quality Factor Q .
- Heterodyne Receiver.
- Image Reject Receiver.

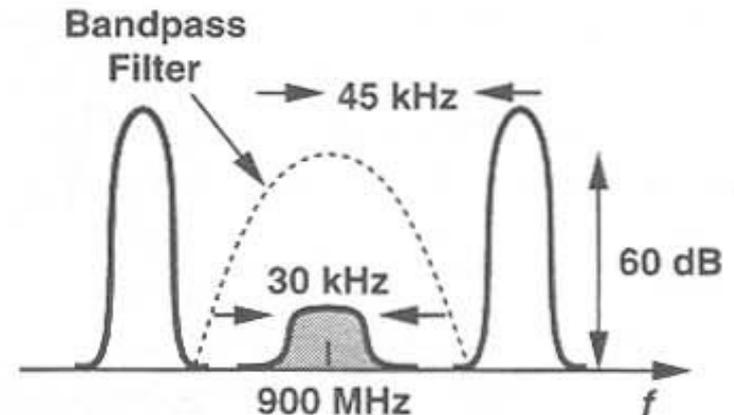
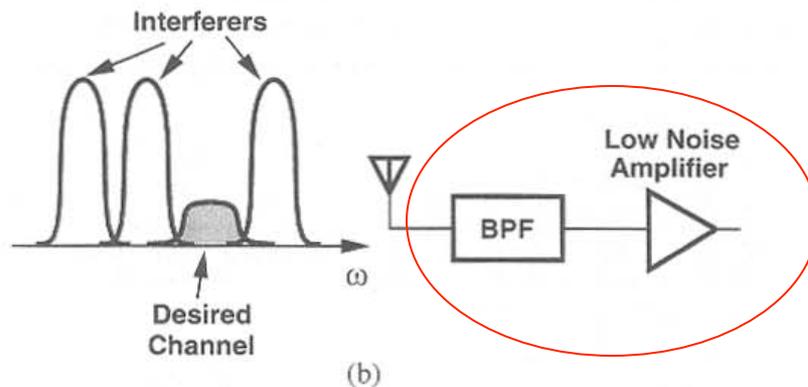
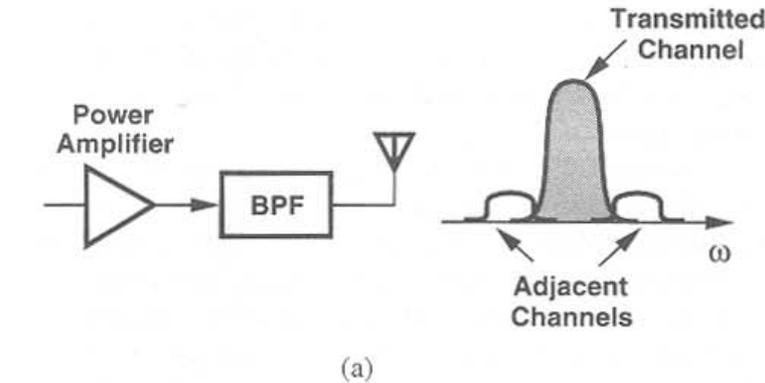
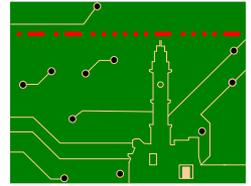


Διάλεξη 4

Most Figures for today's lecture come from:
B. Razavi, RF Microelectronics, Prentice Hall
1998.



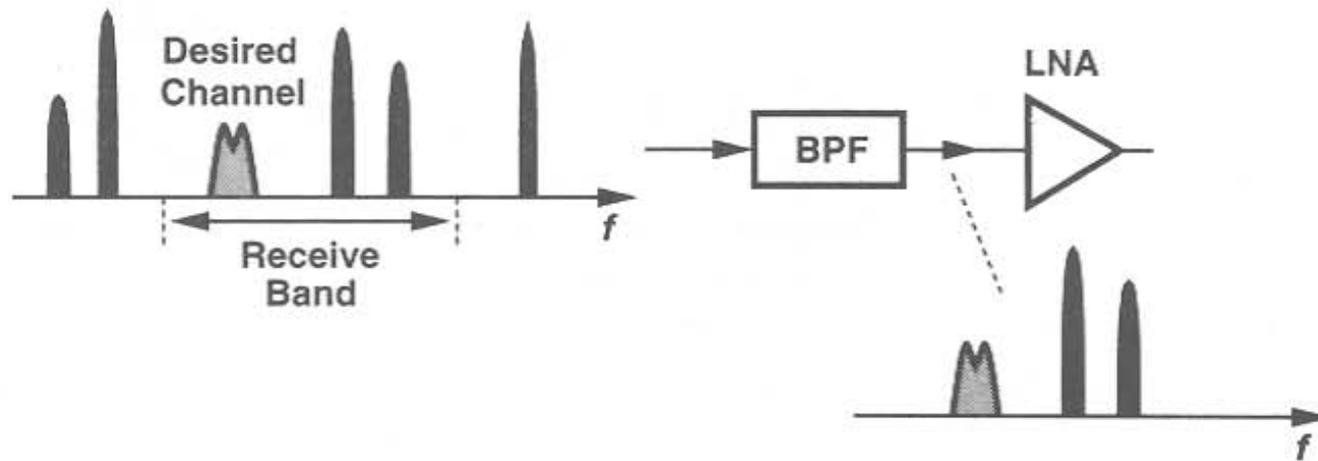
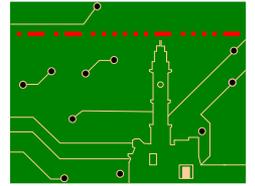
Quality Factor of a Filter



What is the NF of the marked chain?

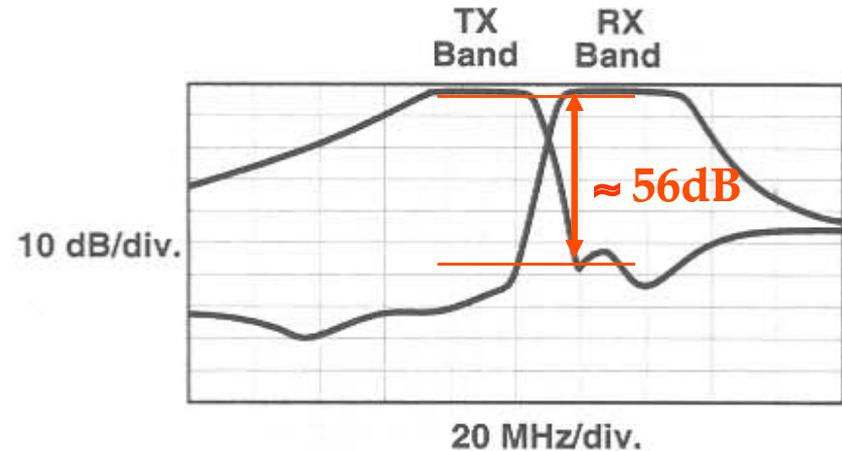
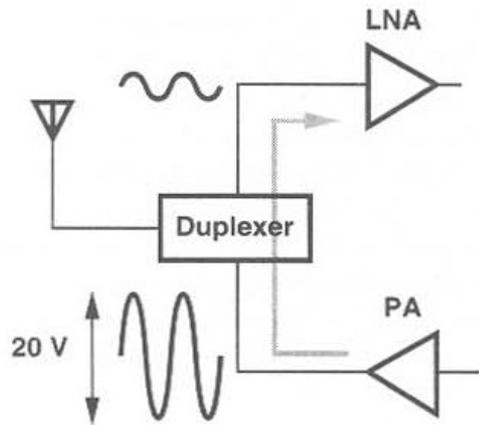
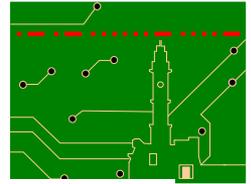
- Filter is needed at both transmit and receive RF-front end.
- $Q = f_c / BW$ (ratio of center frequency with filter bandwidth).
- Q : indication of the complexity (**and cost**) to implement such filter!

Two-step filtering due to Q requirements!



- First filter to grasp the band of interest (several channels)...
- Then filter to focus on the channel of interest...
- Receiver filter Q requirements are relaxed...

Things are not as simple as they look!



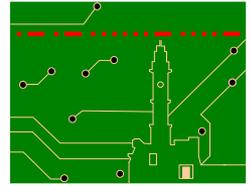
- Filters exhibit Q-loss tradeoff (the higher the Q, the higher the loss)!
Example: filter with 2dB loss amounts to a loss of 369mW for PA output of 1 Watt!

⇒ loss at receiver affects transmitter path.

- Dynamic range on the order of 100dB or more is needed (received signal at the μ V range).

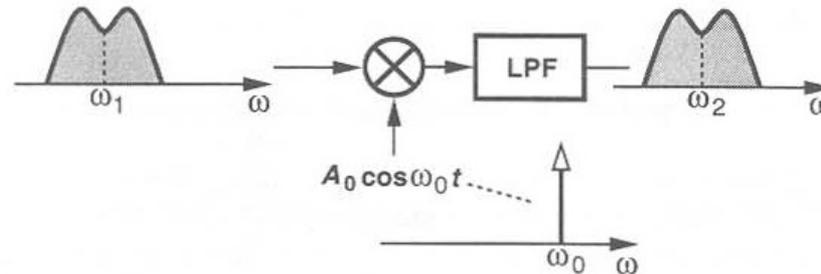
Example: tx 1 W at 50 Ω antenna \Rightarrow 20V_{pp} \Rightarrow
rx leakage = -26dBm = 32mV_{pp} at the rf chain!

Heterodyne Receiver: translation to lower band

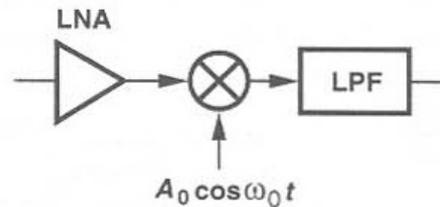


$$\omega_0 \equiv \omega_{LO} = \omega_1 - \omega_2$$

$$\omega_2 = \omega_{IF}$$



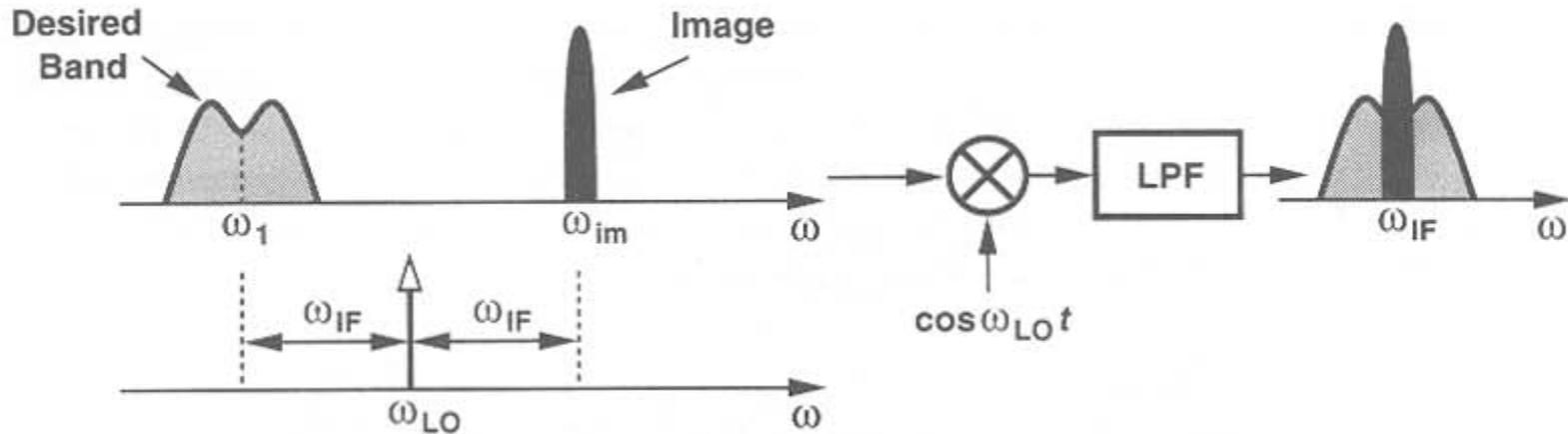
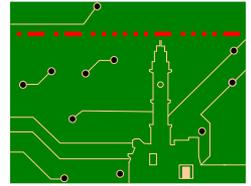
(a)



(b)

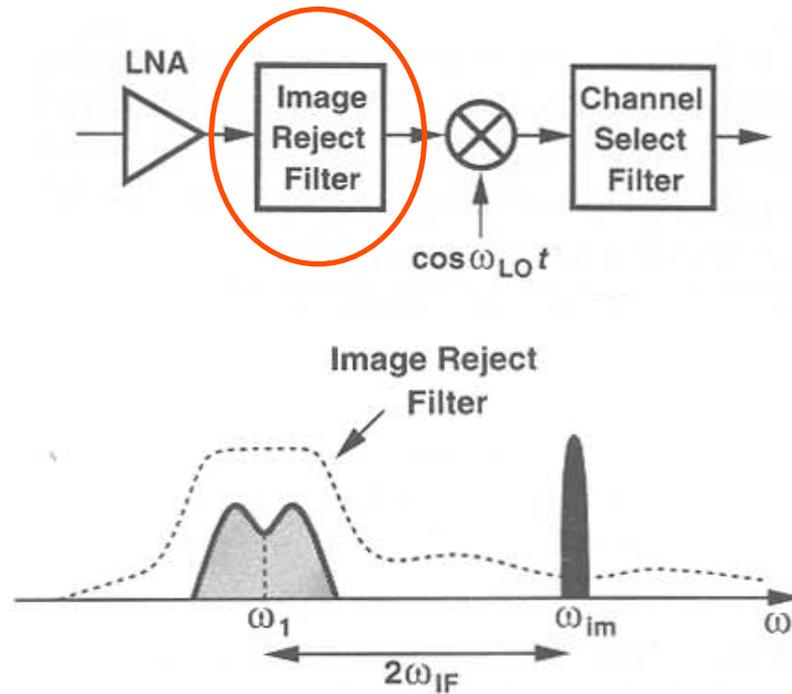
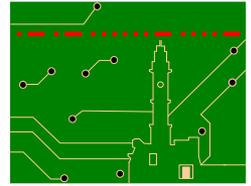
- Translation to lower band (not at DC) eases Q requirements as well as implementation.
- Notice that the component at $|\omega_1 - \omega_{LO}| = \omega_2$ is due to negative freq. of LO.

Heterodyne Receiver: Problem of Image!



- Not only desired freqs are translated...
- Unwanted freqs (images), ω_{IF} away from ω_{LO} , are also translated!
- Serious problem.

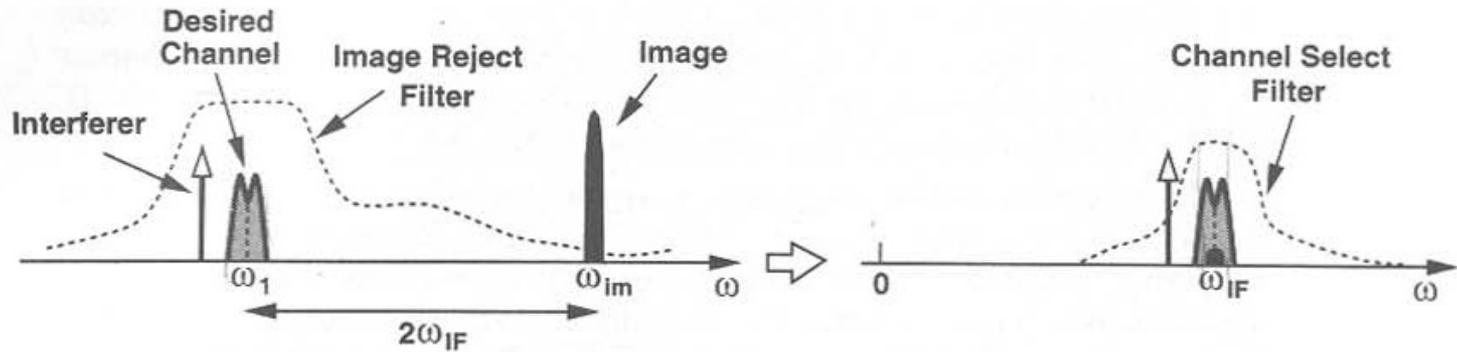
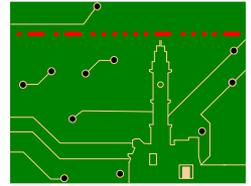
One Solution to the Image Problem: Pre-filtering



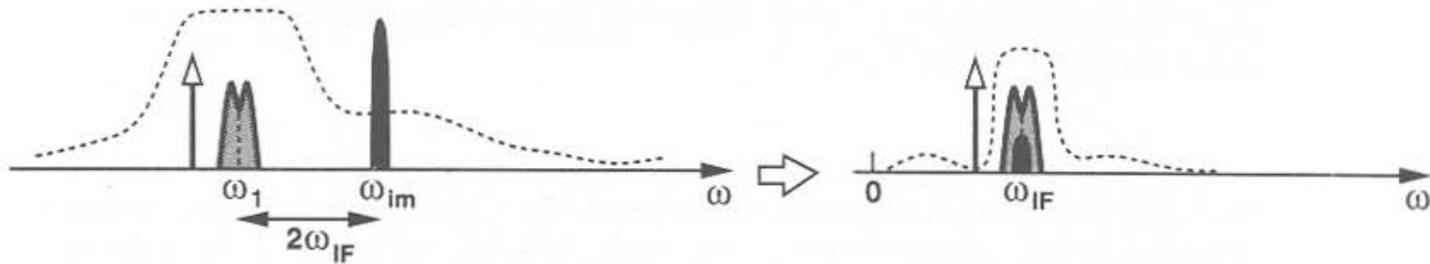
- Using pre-filtering BEFORE mixing, to remove the unwanted image!
- Image Reject filter!

Heterodyne Receiver

Selectivity vs Sensitivity Tradeoff



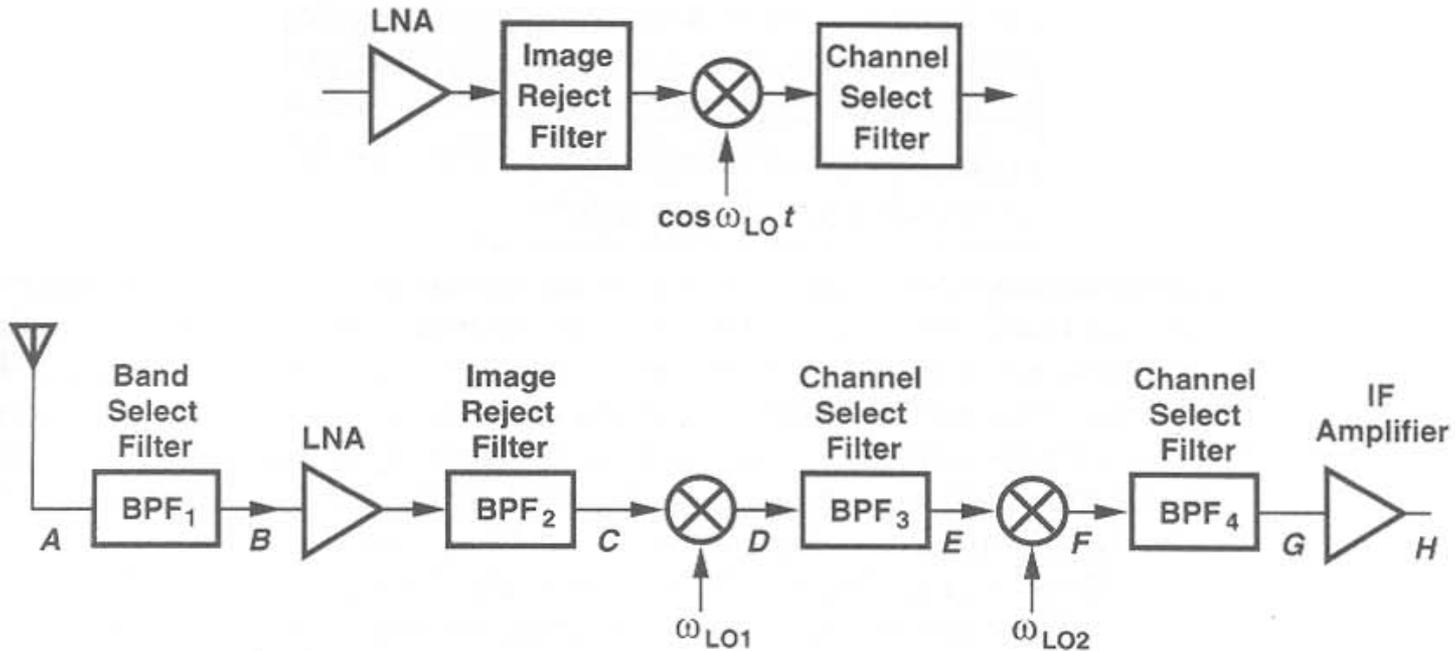
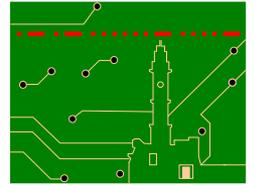
(a)



Not so simple, as it looks:

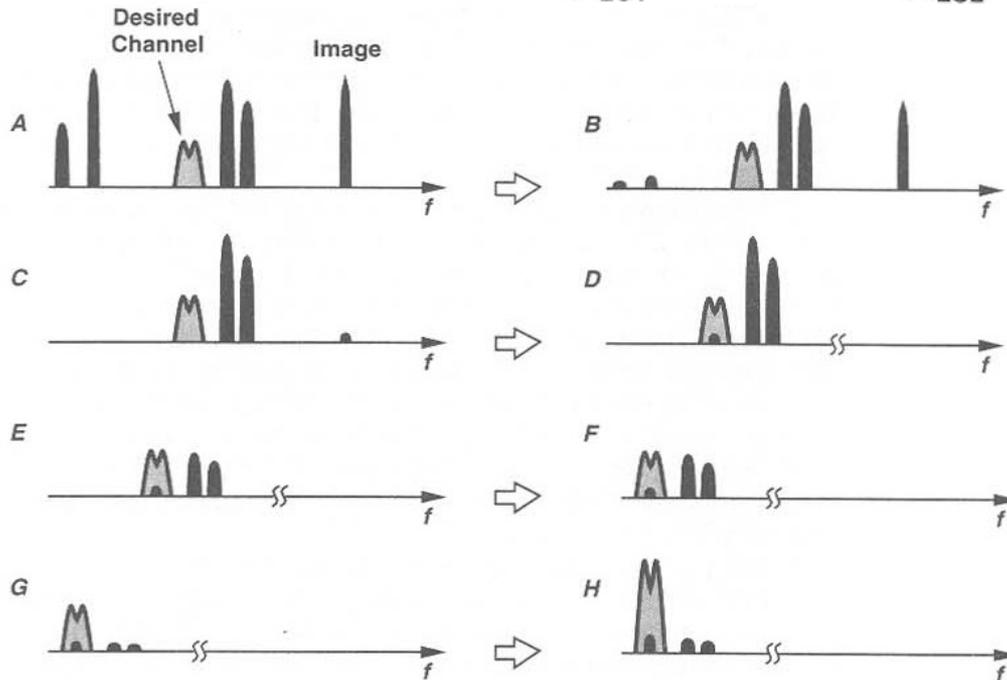
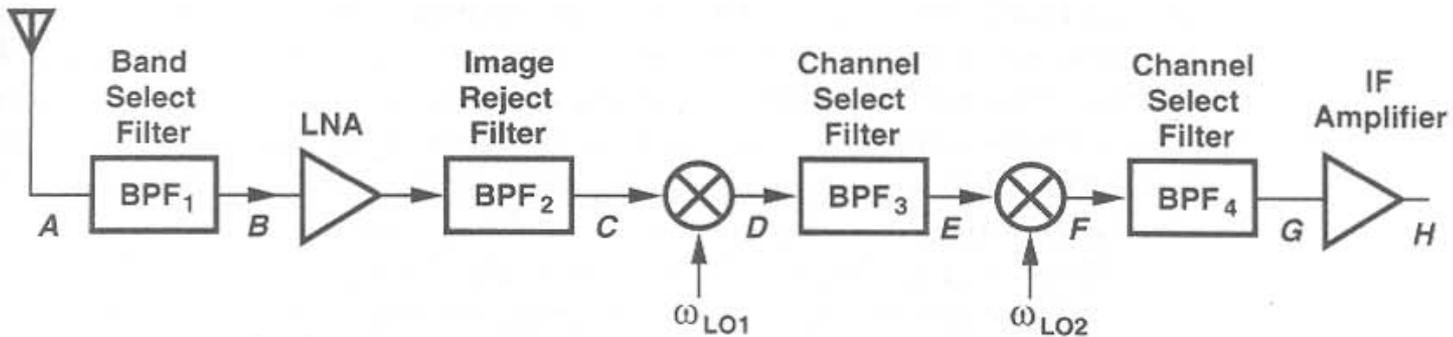
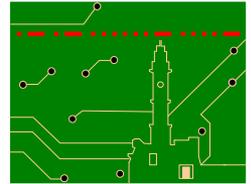
- higher ω_{IF} results to better image rejection (better sensitivity)...
- however, higher ω_{IF} requires higher Q for channel select => practically infeasible => worse channel selection (worse selectivity)!

Addressing the tradeoff: dual-IF topology



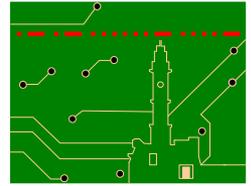
- Two-step conversion (rather than just one)!

Addressing the tradeoff: dual-IF topology

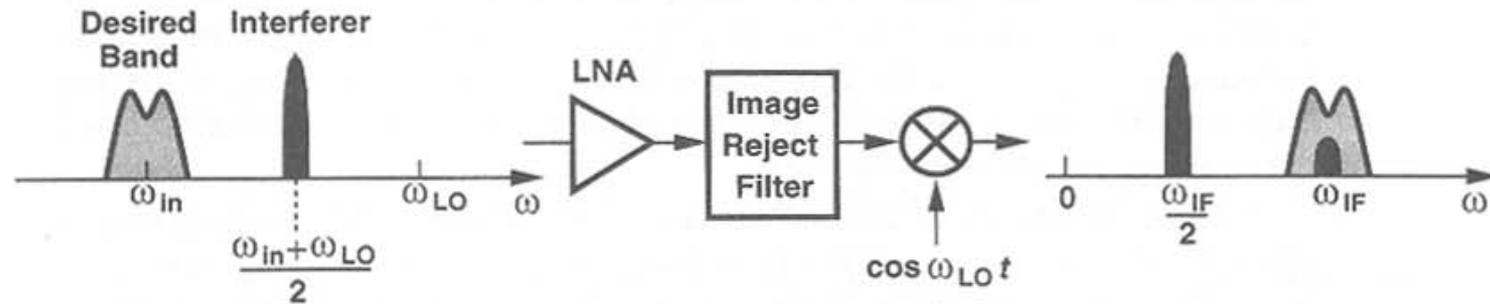


First stage: optimizes for image rejection (sensitivity)

Second stage: optimizes for channel selection (selectivity)



Another Heterodyne Receiver problem: half-IF



- Second order distortion at the RF chain (LNA or mixer):

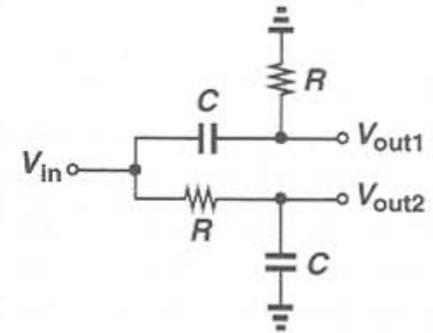
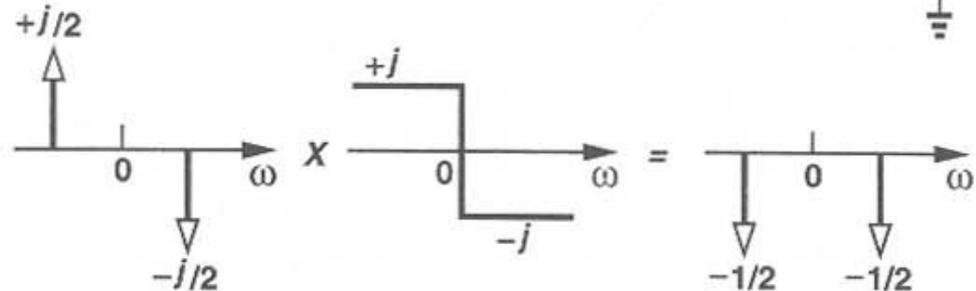
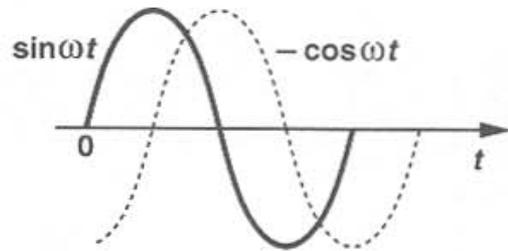
$$\frac{\omega_{in} + \omega_{LO}}{2} \Rightarrow \omega_{in} + \omega_{LO} \quad \Rightarrow 2\omega_{LO} - (\omega_{in} + \omega_{LO}) = \omega_{LO} - \omega_{in} = \omega_{IF}$$

$$\omega_{LO} \Rightarrow 2\omega_{LO}$$

- ...or interferer at $\omega_{IF}/2$ and second order distortion at the RF chain.

- Solution: minimize second order distortion and/or filtering.

Another solution to the Image Problem: Image Reject Receiver

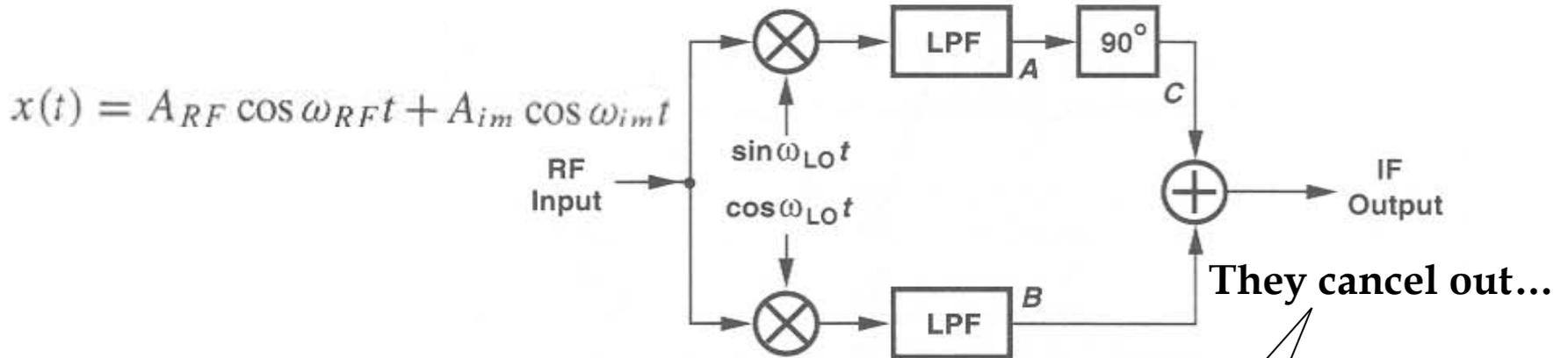
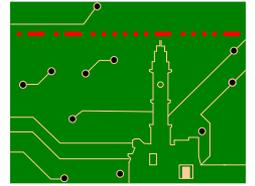


- Basic idea: process signal and image DIFFERENTLY (and eventually cancel out the image).
- Mechanism: Hilbert Transform or “shift by 90°”!

$$H(\omega) = -j \operatorname{sgn}(\omega)$$

- In practice, $\cos(\omega t)$ is converted to $\sin(\omega t)$ and $\sin(\omega t)$ to $-\cos(\omega t)$ (shift by $(t-T/4)$)

Image Reject Receiver: Hartley Architecture



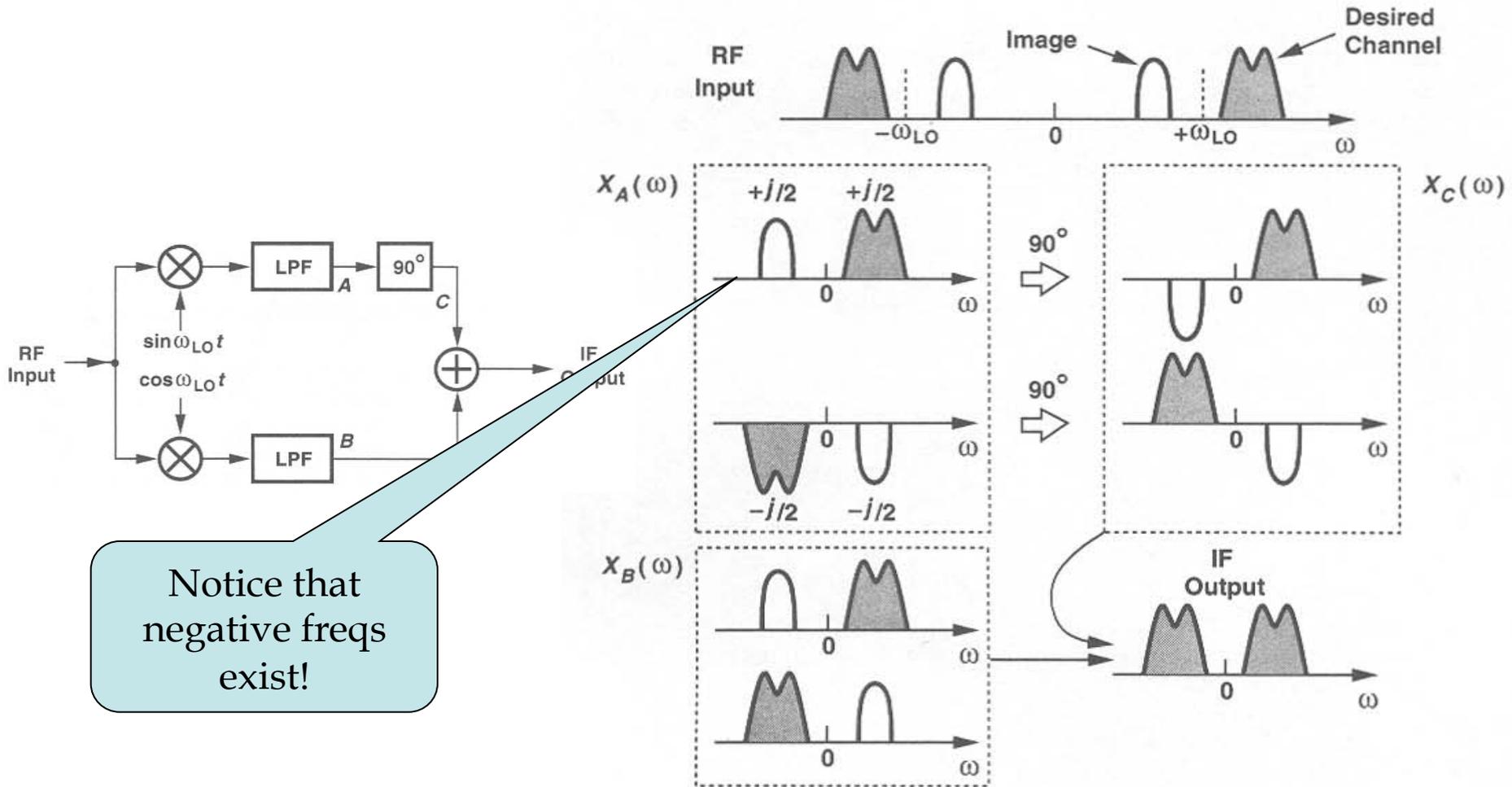
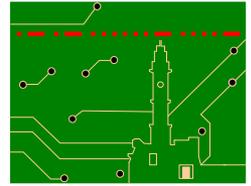
$$x_A(t) = \frac{A_{RF}}{2} \sin(\omega_{LO} - \omega_{RF})t + \frac{A_{im}}{2} \sin(\omega_{LO} - \omega_{im})t$$

$$x_B(t) = \frac{A_{RF}}{2} \cos(\omega_{LO} - \omega_{RF})t + \frac{A_{im}}{2} \cos(\omega_{LO} - \omega_{im})t$$

$$x_A(t) = -\frac{A_{RF}}{2} \sin(\omega_{RF} - \omega_{LO})t + \frac{A_{im}}{2} \sin(\omega_{LO} - \omega_{im})t$$

$$x_C(t) = +\frac{A_{RF}}{2} \cos(\omega_{RF} - \omega_{LO})t - \frac{A_{im}}{2} \cos(\omega_{LO} - \omega_{im})t$$

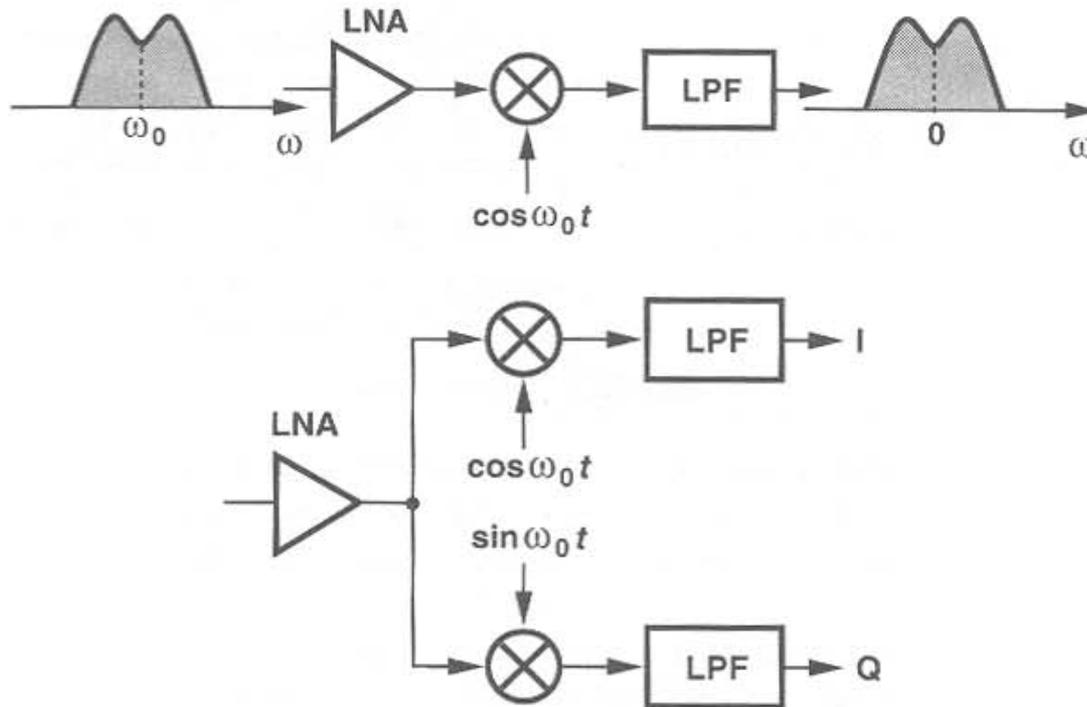
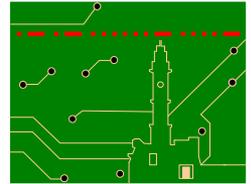
Image Reject Receiver: Hartley Architecture (graphical representation)



Notice that
negative freqs
exist!

- Hartley architecture is sensitive to LO phases mismatch.

Homodyne (zero-IF) Receiver



- Directly convert to DC ($\omega_{LO} = \omega_{in} = \omega_1$, $\omega_{IF} = 0$).
- Why don't we use zero-IF instead of heterodyne rec?

(answer at next lecture)

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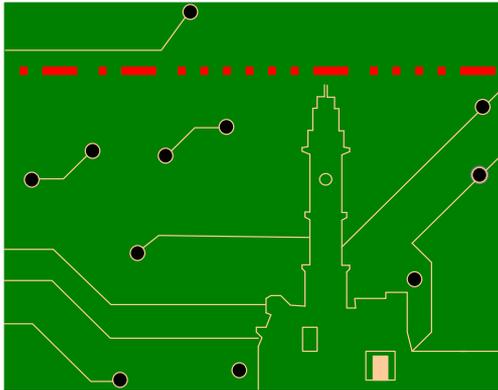
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Questions?



Next lecture: homodyne receivers and transceiver architectures (cont'd)